

# Novel 3-D Differential Phase Contrast Imaging

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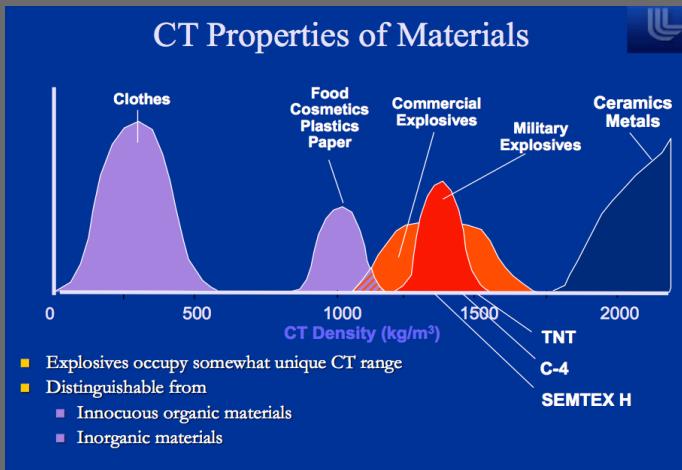
# Acknowledgments

- We are grateful for support from the DHS S&T under grant:  
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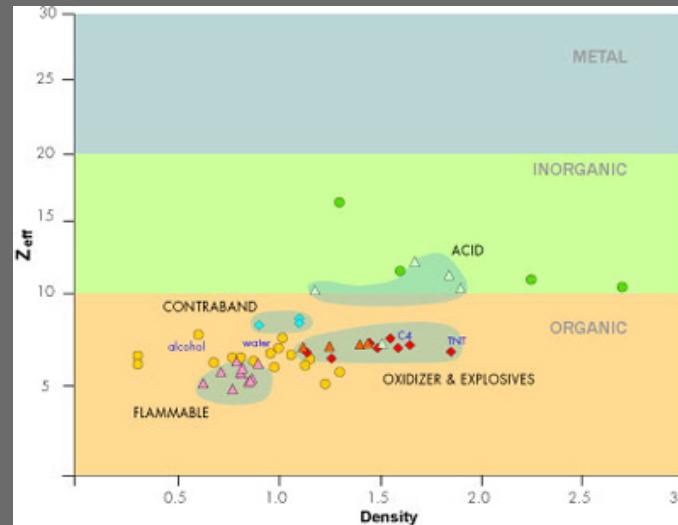
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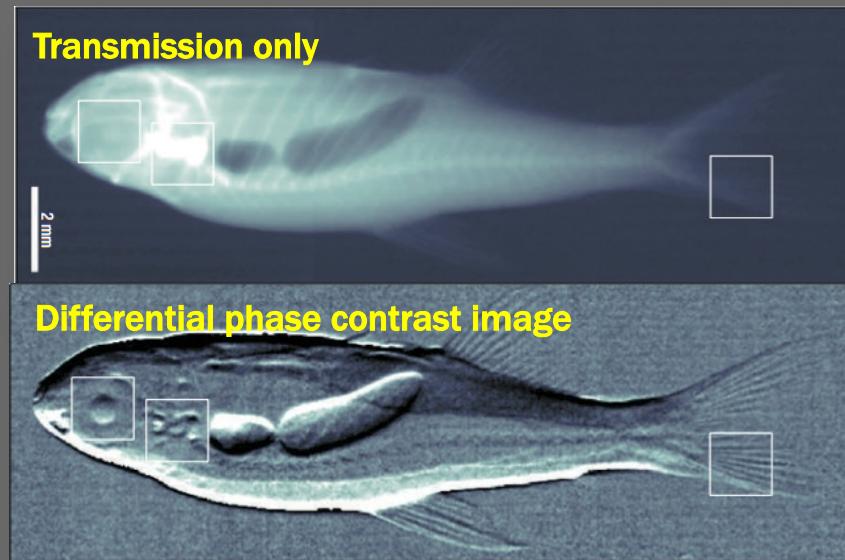
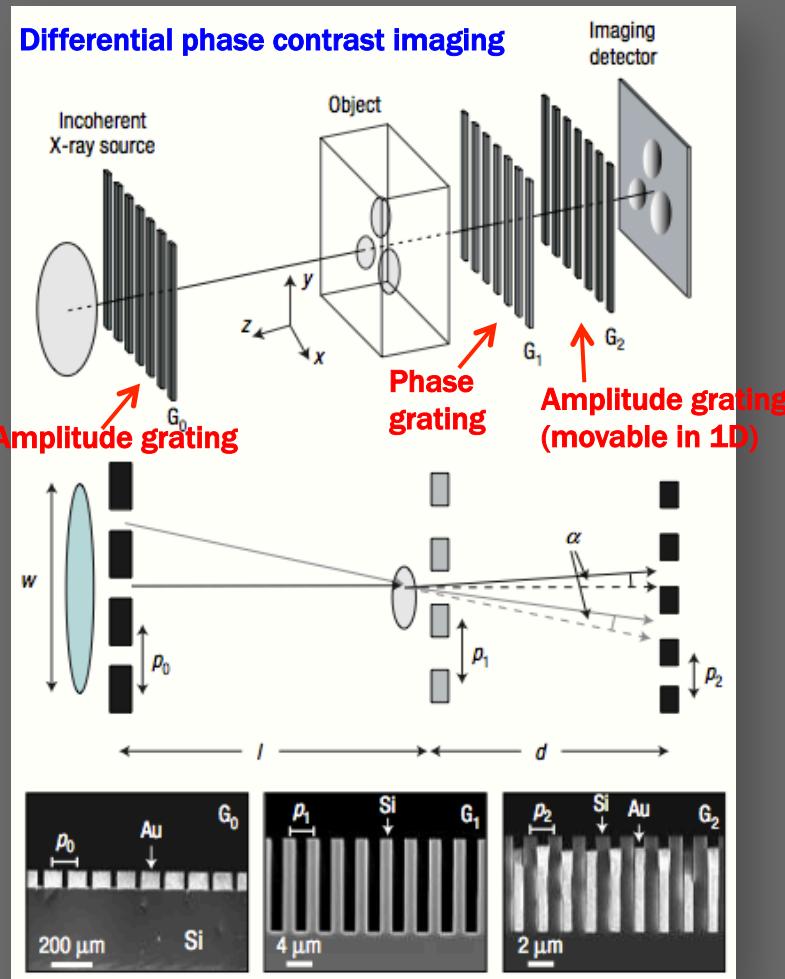
# Introduction: Problem Statement



H. Martz, C. Crawford, Explosives detection in aviation applications using CT, LLNL, June 2010



# X-ray Differential Phase-Contrast Imaging

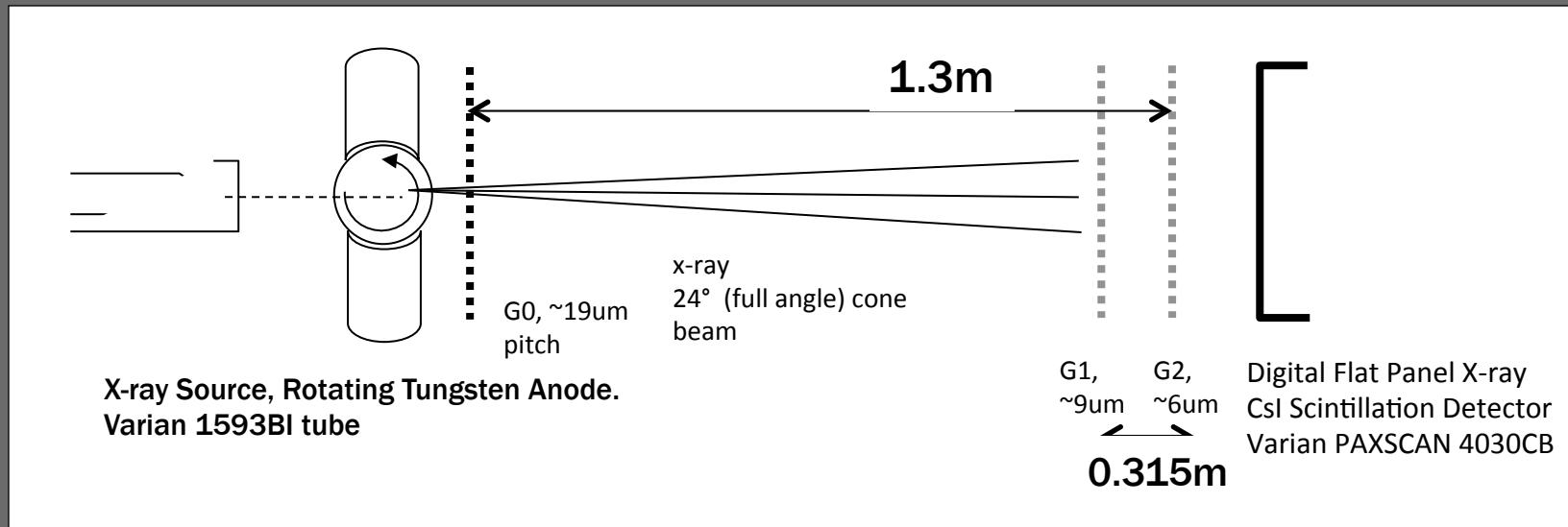


Pfeiffer et al., Nature Phys.. (2006)

## Challenges:

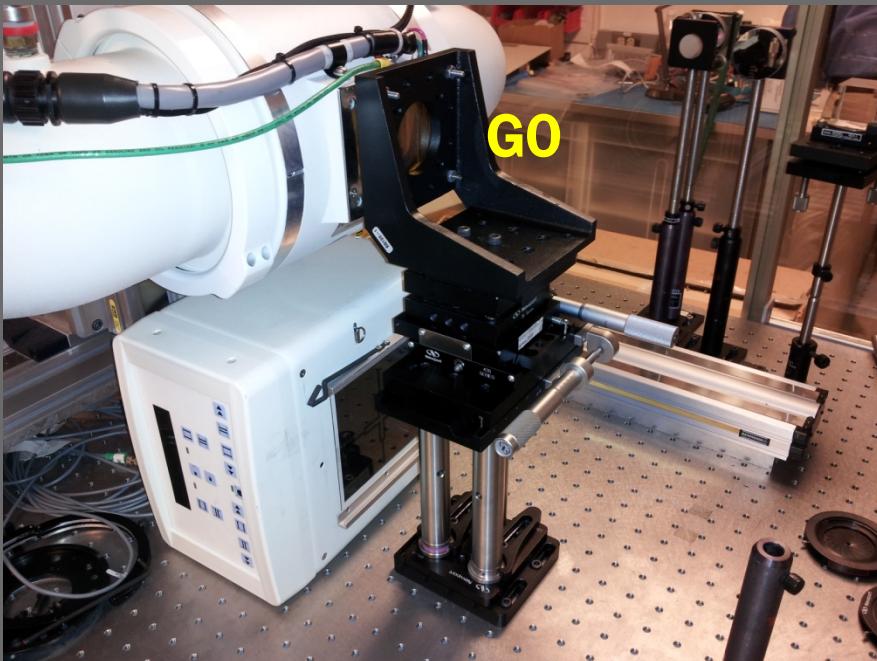
- Need high aspect-ratio (> 100X) amplitude grating for high energy (> 100 keV) X-ray design.

# Experimental Schematic

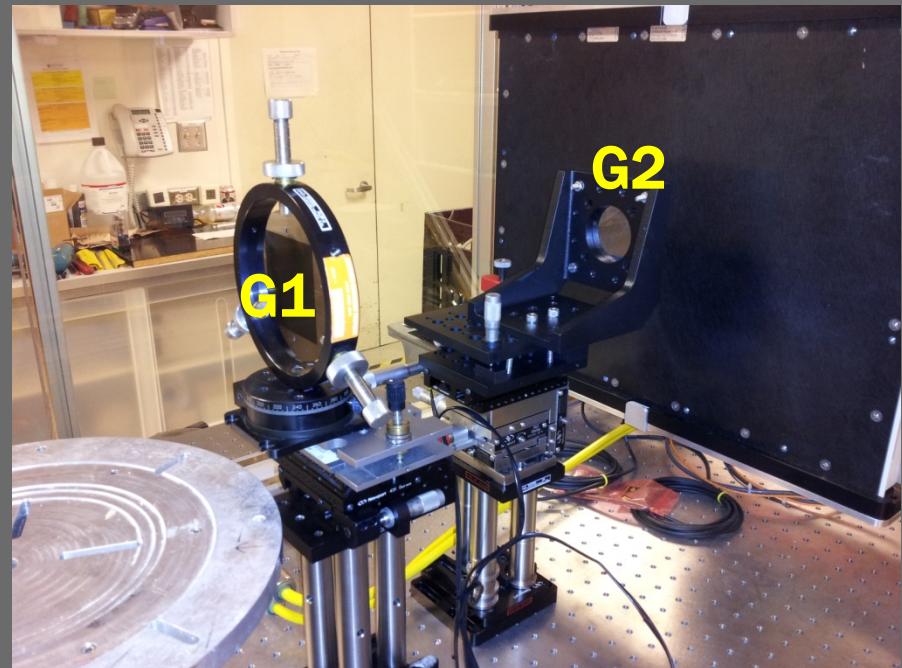


- Incoherent, polychromatic source is made partially coherent by grating G0.
- G1 and G2 form a phase grating/amplitude grating interferometer analyzer pair.
- G0-G2 distance = 1.3m, G1-G2 distance 0.315m, G0=19um, G1=9um, G2=6um.
- Phase contrast signal is detected at the digital flat panel detector.
- X-ray parameters: 60kVp, 10mA, 7.5pps. Detector: 1x1 0.5pF Gain 2

# Photos of the Setup



G0, on x-y stage

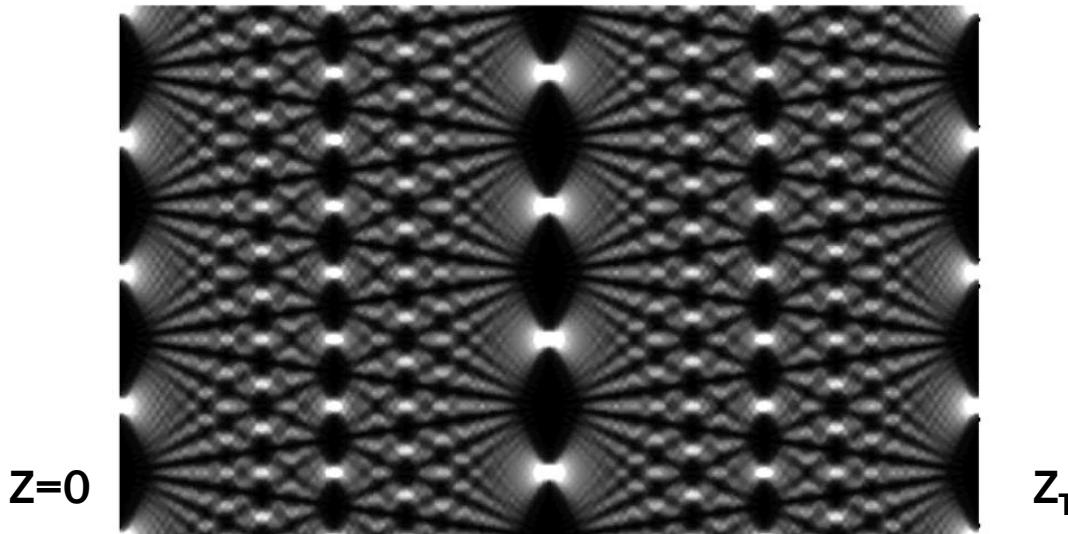


G1, on x-y and tilt/rotation stage  
G2, on x-y-z and tip/tilt/rotation  
stage+ pico motor drive

# X-ray Talbot Interferometry

- Uses Talbot effect for G1 and G2 gratings.
- Moiré Pattern detection at detector.
- Partial Coherence needed, G0 provides this via van Cittert-Zernike Theorem (Think Ducks).
- G1 can be Phase or Amplitude.
- Works with polychromatic sources.

# The Talbot Effect



$z=0$

$z_T$

$$E(x, z) = C \int e^{\frac{i}{2z}(x-x')^2} E(x', 0) dx'$$

$$E(x, 0) = T(x) = \sum_n a_n e^{\frac{i}{p_0} nx}$$

$$E(x, z) = C \sum_n a_n \int e^{\frac{i}{2z}(x'-x)^2} e^{\frac{i}{p_0} nx'} dx'$$

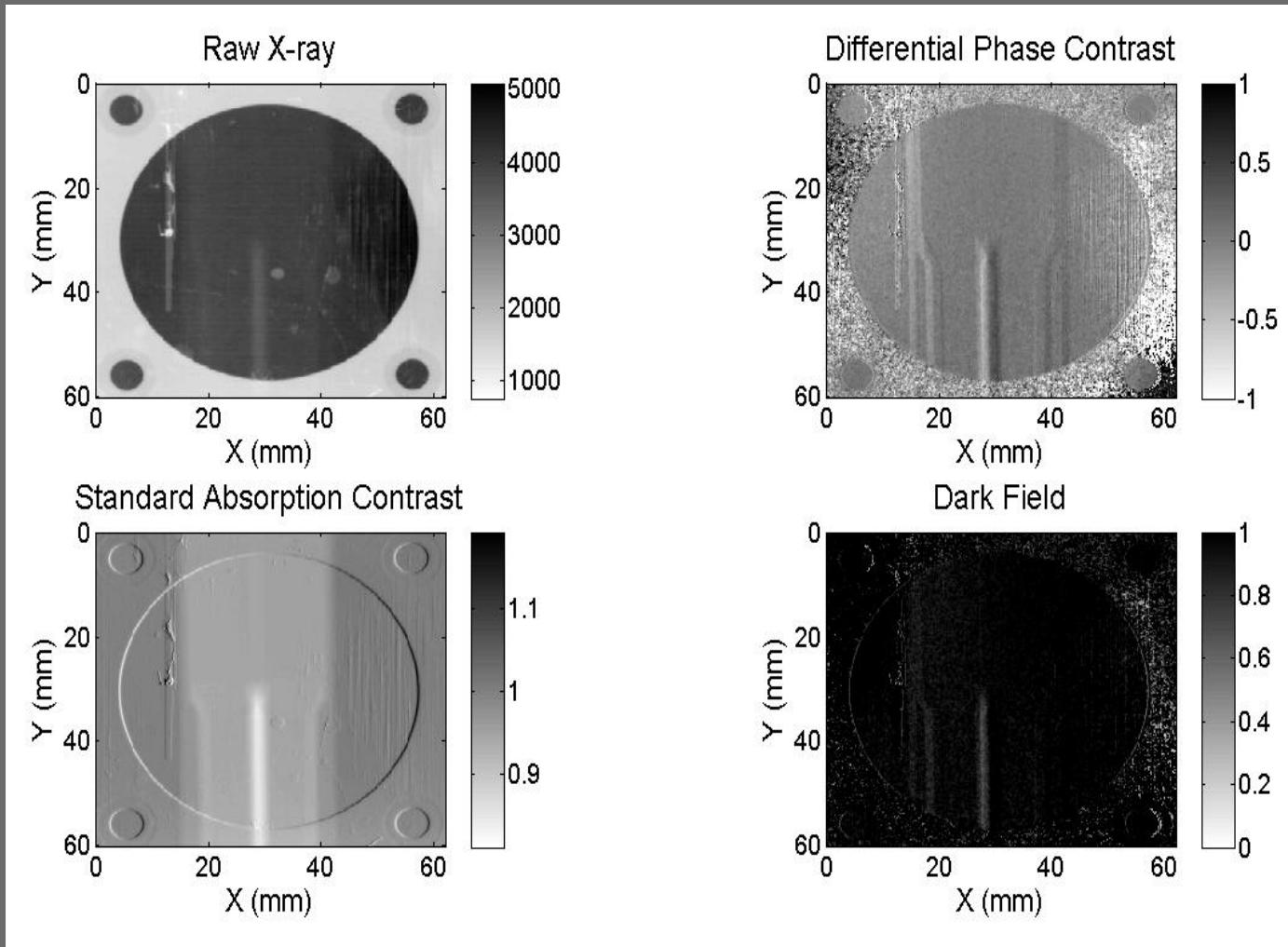
$$E(x, z) = C' \sum_n a_n e^{\frac{i}{p_0} nx} e^{-i \frac{\pi \lambda z}{p_0^2} n^2}$$

$$2\pi m = \frac{\pi \lambda z}{p_0^2}$$

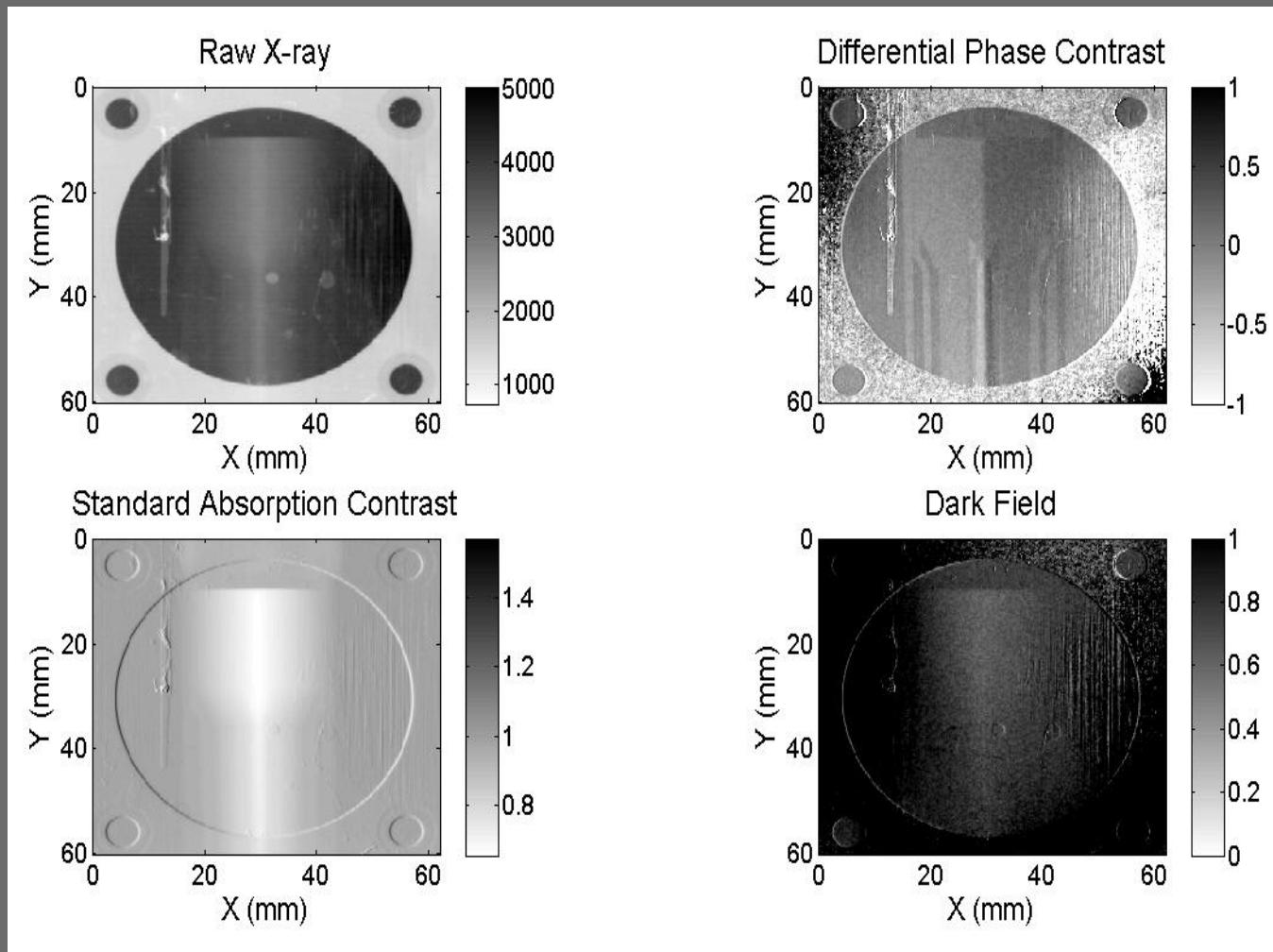
$$z = mz_T$$

$$z_T = \frac{2p_0^2}{\lambda}$$

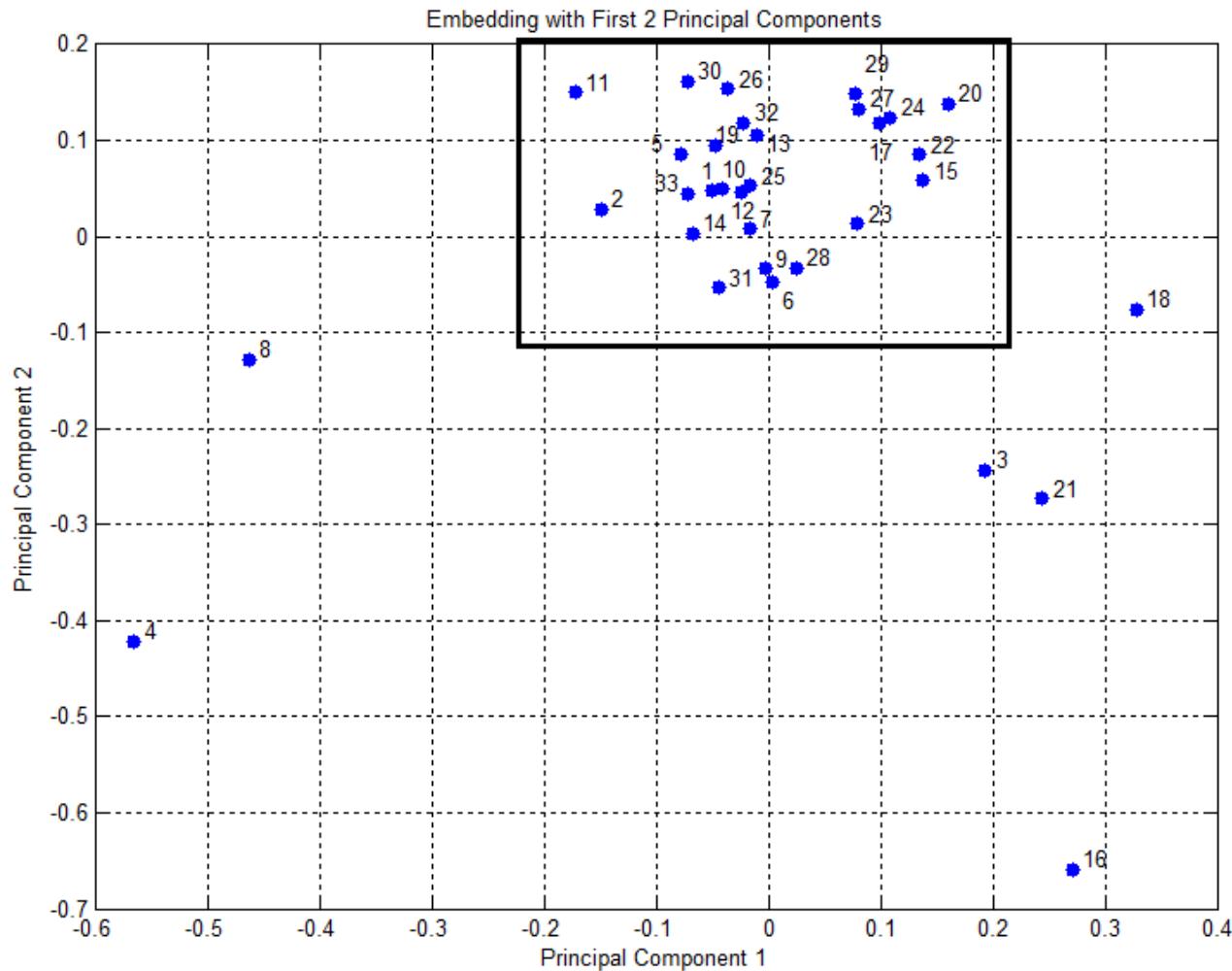
# X-ray Absorption, DPC, and Dark Field Contrast Images of Empty Cuvette



# X-ray Absorption, DPC, and Dark Field Contrast Images of Water + Cuvette

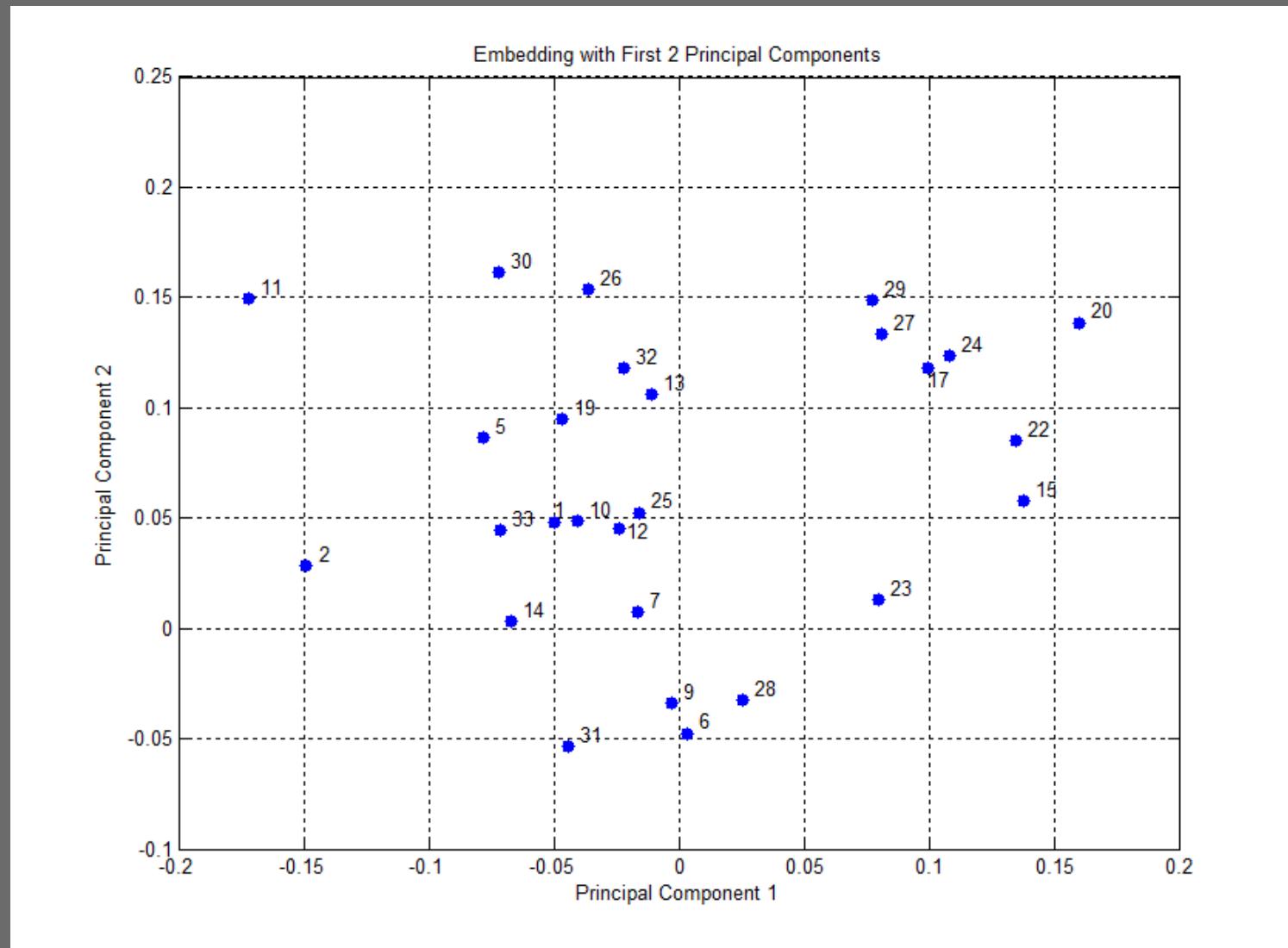


# Principal Component Analysis

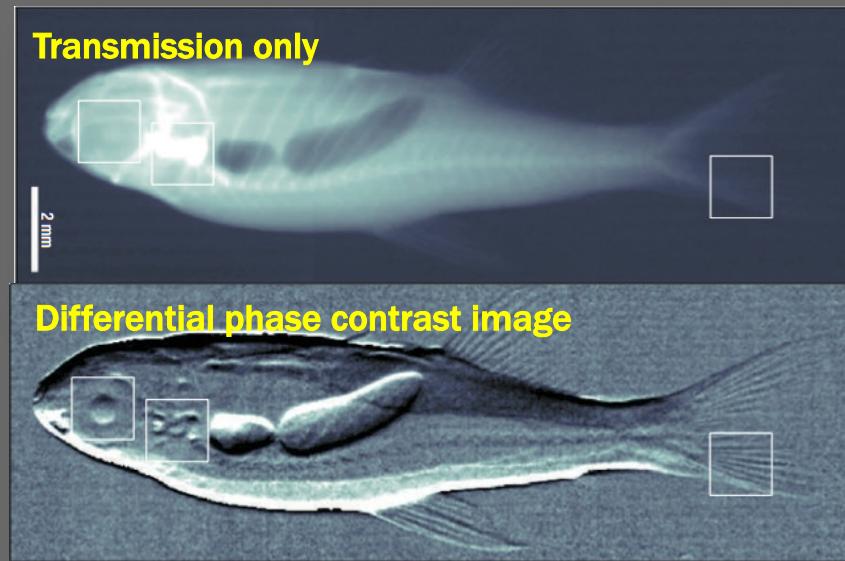
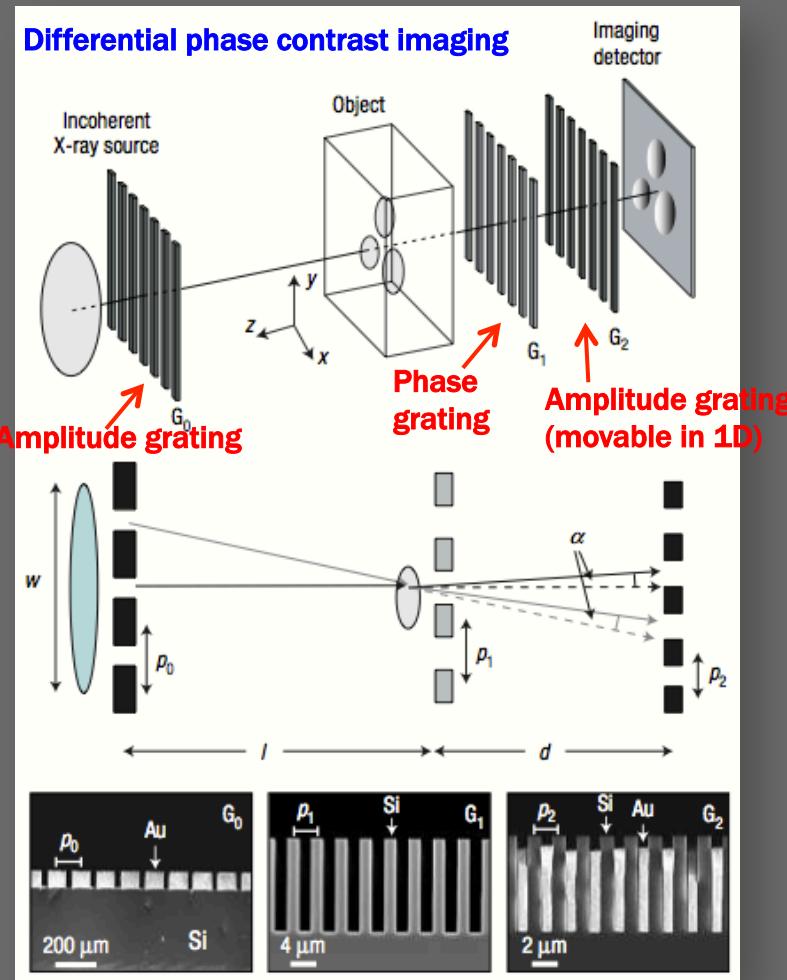


Squared area shows in next figure

# Principal Component Analysis



# X-ray Differential Phase-Contrast Imaging



## Problems:

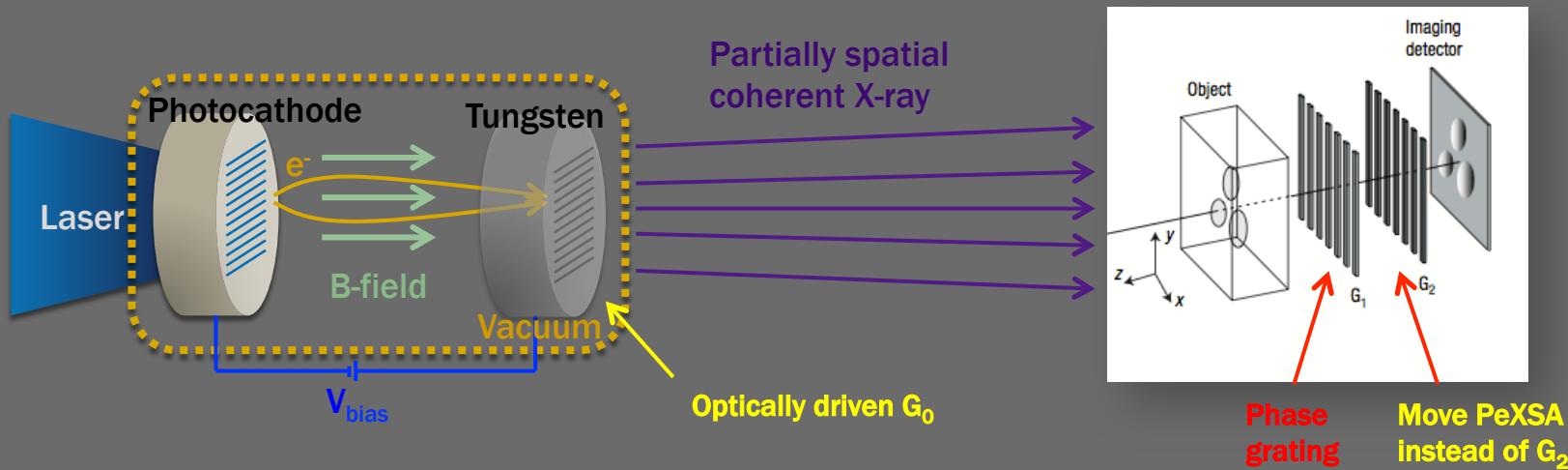
- Amplitude grating  $G_0$  blocks > 75% of incident X-rays (for spatial coherence).
- Need high aspect-ratio (> 100X) amplitude grating for high energy (> 100 keV) X-ray design.

# Solution

## *Optically Driven Patterned X-ray Source*

### Photoelectron X-ray Source Array (PeXSA)

We can reduce the wasted X-ray power > 4X and  
replace the tricky high aspect ratio amplitude grating

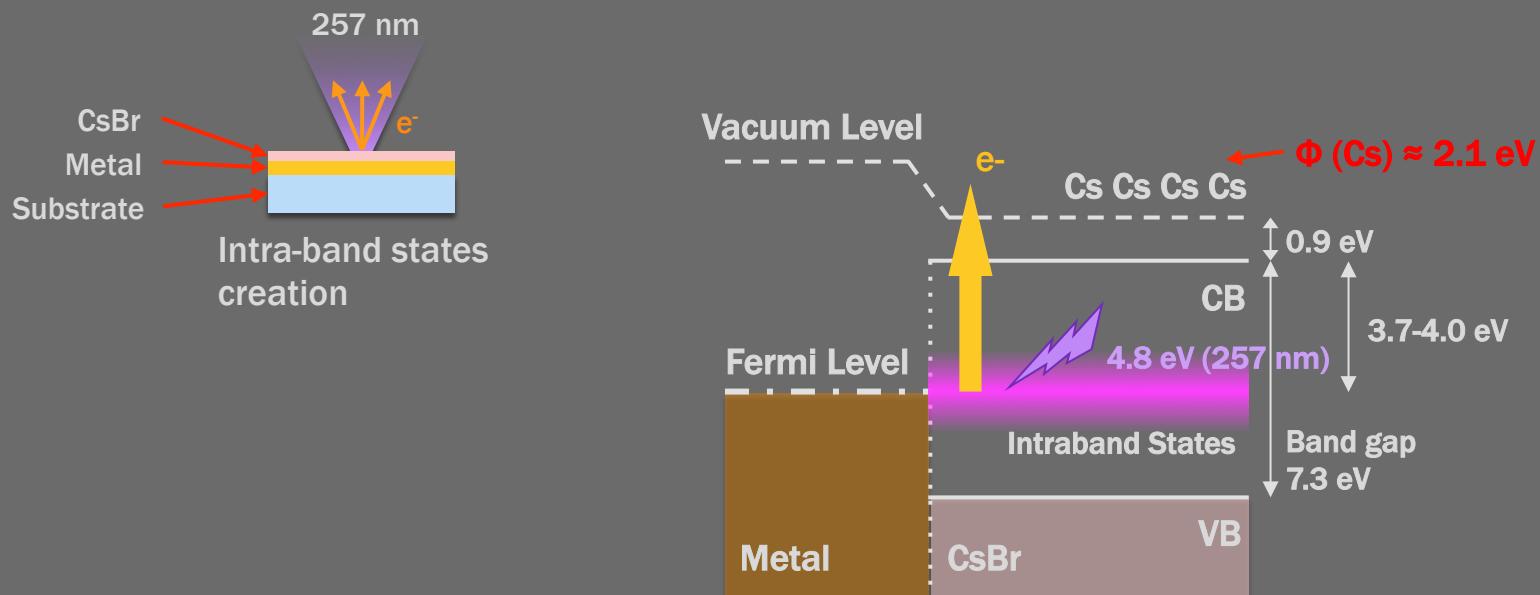


A spatial light modulator now generates the optical pattern  
... hence the e-beam pattern  
... hence the X-ray pattern  
G<sub>2</sub> grating does not need to move!

Ongoing research

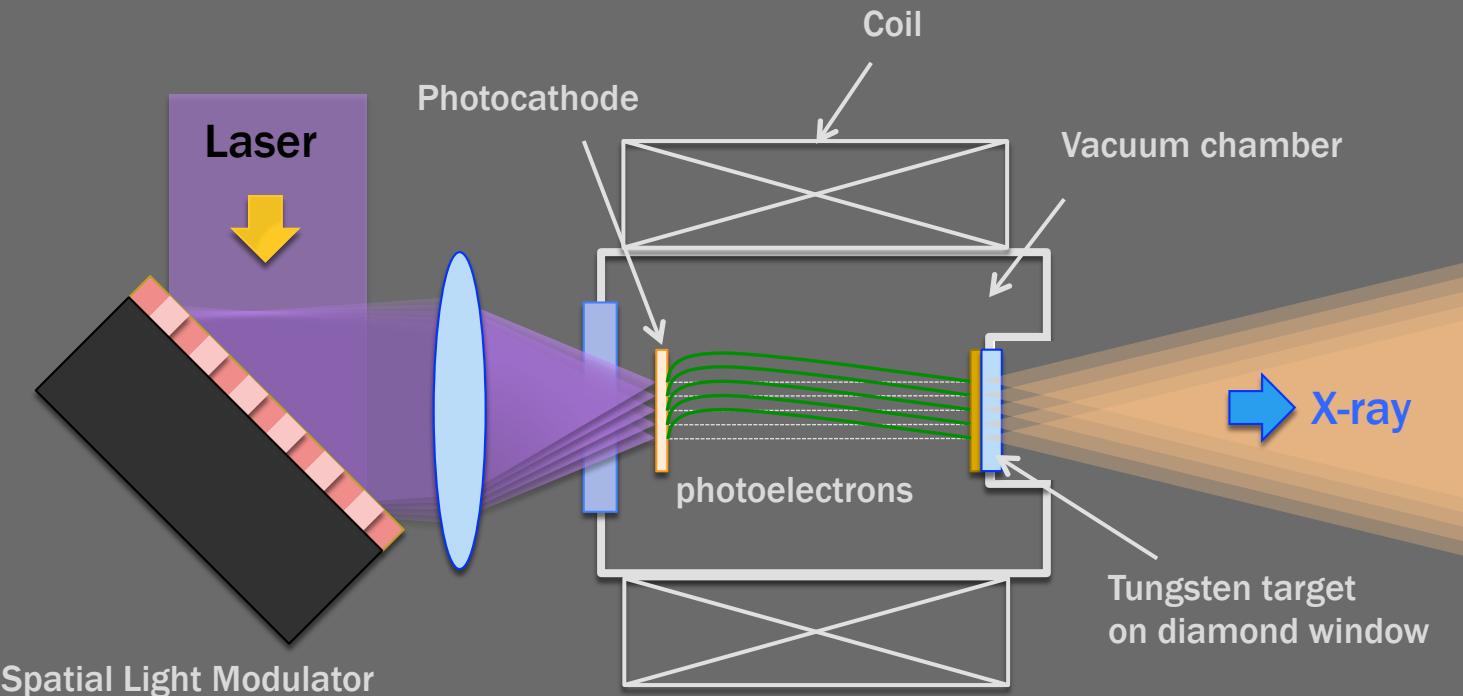
# Photoelectron Source

## UV activated intraband states in CsBr

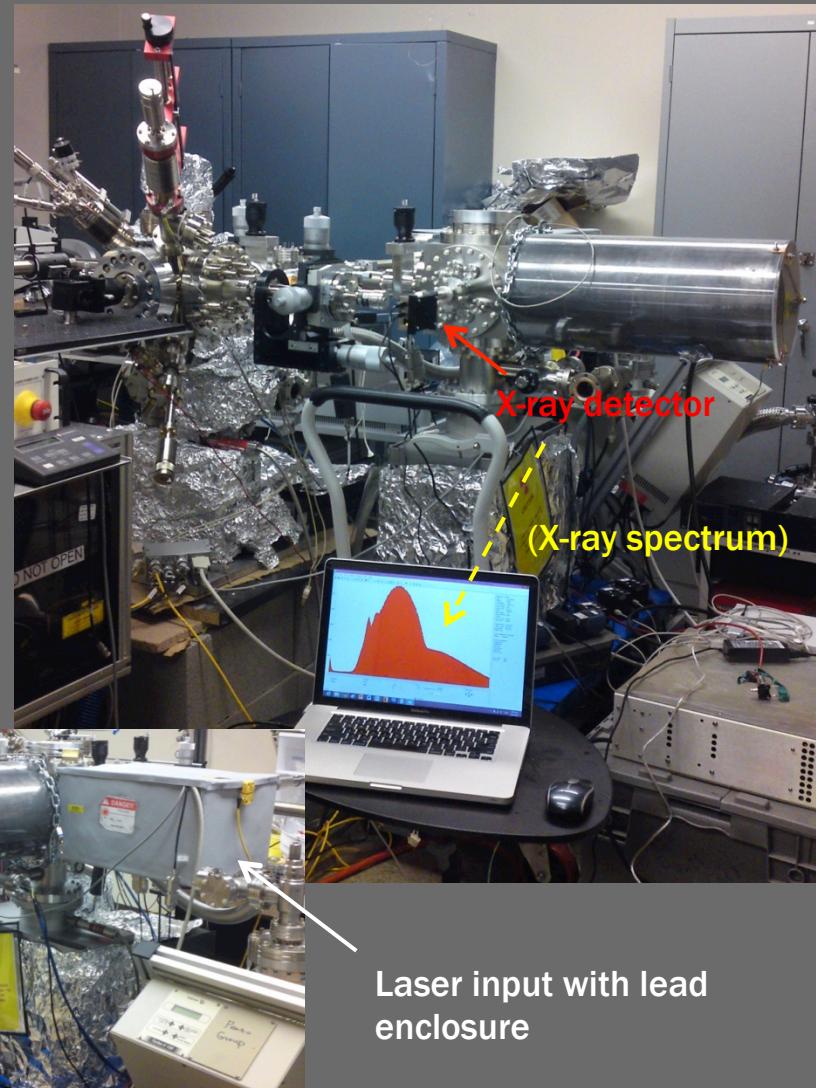
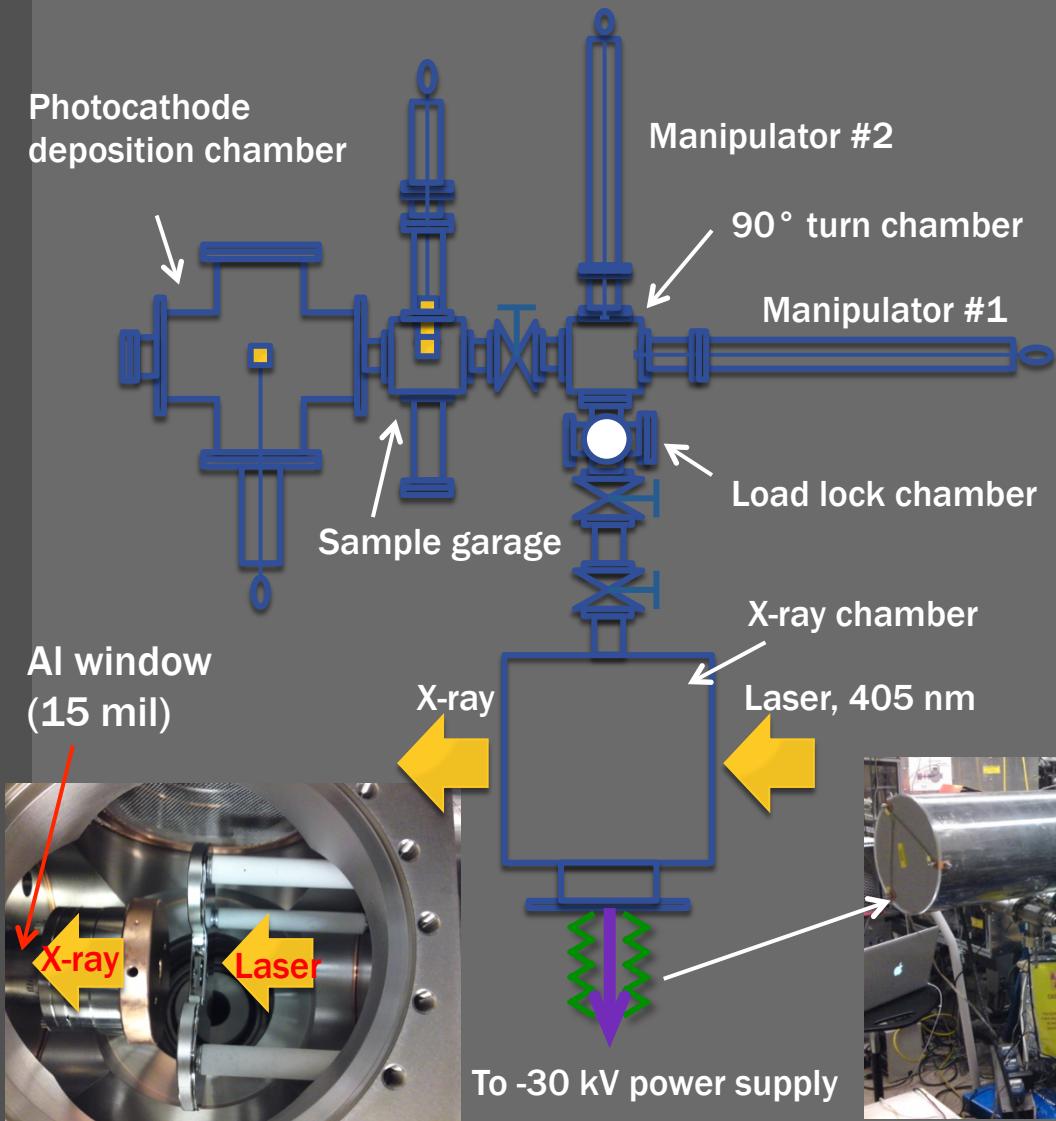


Use UV to activate intra-band states first.

# Photoelectron X-ray Source Array

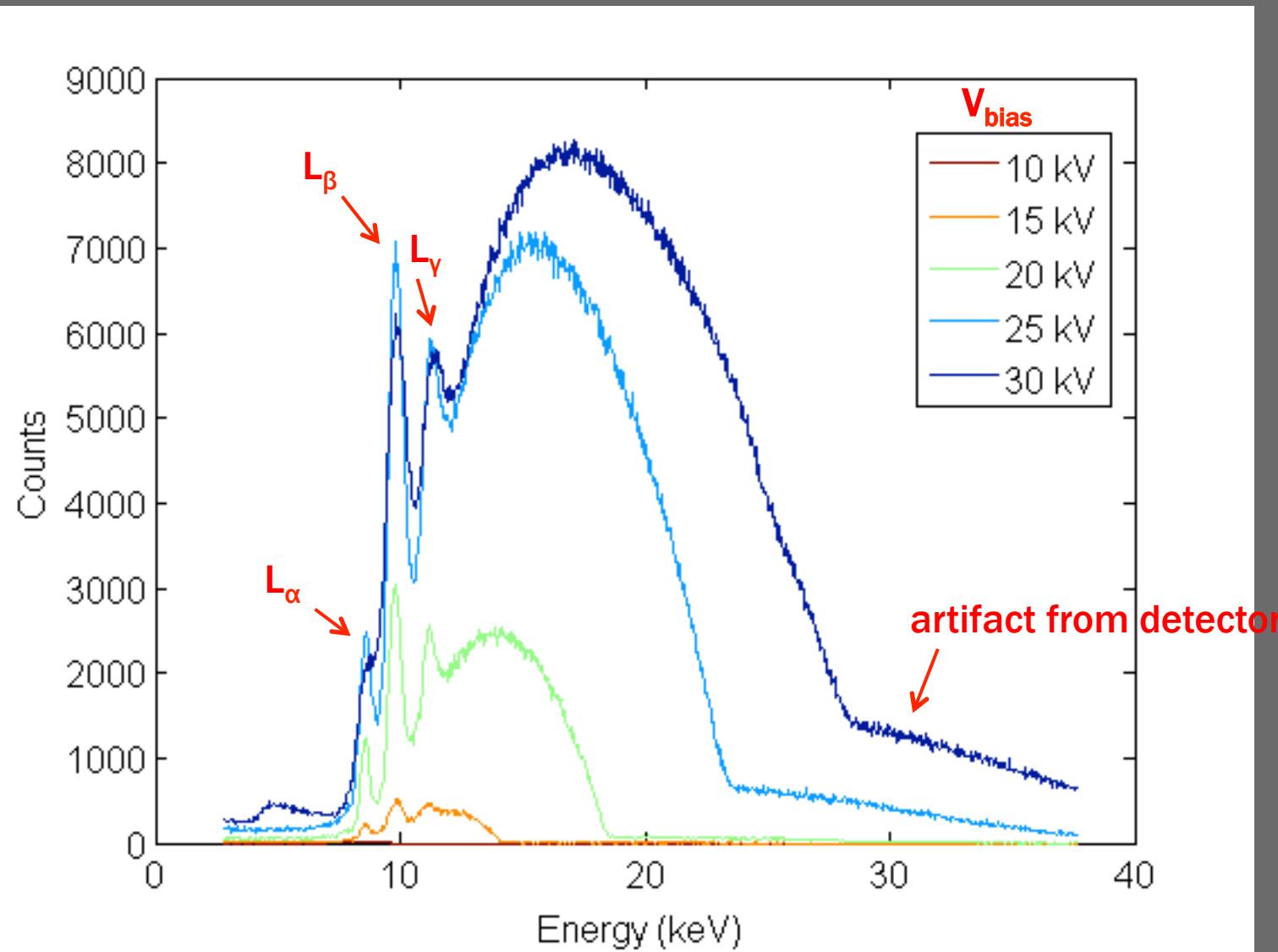


# PeXSA Setup



# Photoelectron Excited X-ray

Transmission W target, Laser power 5 mW,  $V_{bias}$  10 kV-30 kV



# Summary

- DPC measurements provide richer detection signatures
  - *More work to be done to determine effectiveness within cluttered bag*
- *Photo Electron X-ray Source Array (PeXSA) enables simpler and more sensitive DPC system with large FoV*
  - *Gratings severely limit FoV for high energy system*